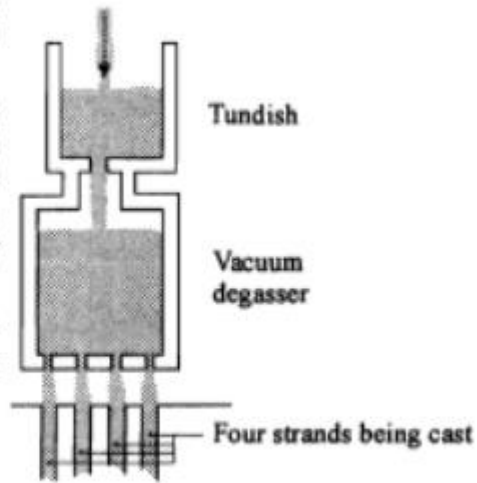


**4.16** In planning continuous casting, we use fluid flow analysis. Consider the illustrated configuration of the equipment, which includes in-line vacuum degassing.



a) Determine the tundish and degasser nozzle sizes which are necessary to operate the system at a rate of  $6.3 \text{ kg s}^{-1}$  per strand. Suppose that for operational reasons it is desirable to maintain tundish and degasser bath depths of  $0.76$  and  $1.83 \text{ m}$ , respectively.

b) If only  $13 \text{ mm}$  diameter degasser nozzles are available, how would their use affect the casting operation?

*Inside dimensions:* tundish,  $2.4 \text{ m} \times 2.4 \text{ m} \times 1.2 \text{ m}$ ; degasser,  $1.2 \text{ m} \times 1.2 \text{ m} \times 2.4 \text{ m}$ .

Liquid-steel density =  $7530 \text{ kg m}^{-3}$ .

Discharge coefficients for tundish and vacuum degasser nozzles:  $C_D = 0.8$ .

Vacuum pressure =  $10^{-3} \text{ atm}$  ( $101 \text{ N m}^{-2}$ ).

$$(a) \quad W := 4 \cdot 6.3 \cdot \frac{\text{kg}}{\text{s}} \quad h := -0.76 \cdot \text{m} \quad \rho := 7530 \cdot \frac{\text{kg}}{\text{m}^3} \quad C_D := 0.8 \quad P_2 := 101 \cdot \text{Pa} \quad \beta := 1$$

$$v_2 := \sqrt{2} \cdot C_D \cdot \left( -\frac{(P_2 - 1 \cdot \text{atm})}{\rho} - g \cdot h \right)^{0.5} = 5.172 \frac{\text{m}}{\text{s}} \quad d := \sqrt{\frac{W}{v_2 \cdot \pi \cdot \rho}} = 14.352 \text{ mm}$$

Check:

$$\frac{(P_2 - 1 \cdot \text{atm})}{\rho} + \frac{v_2^2}{2} \frac{1}{C_D^2} + g \cdot h = 0 \frac{\text{m}^2}{\text{s}^2}$$

(b) If  $d = 13 \text{ mm}$  Increase the head to  $1.794 \text{ m}$  to maintain the required flow rate.

$$W_{13} := W \cdot \left( \frac{13 \cdot \text{mm}}{d} \right)^2 = 20.676 \frac{\text{kg}}{\text{s}} \quad v_{13} := v_2 \cdot \left( \frac{d}{13 \cdot \text{mm}} \right)^2 = 6.303 \frac{\text{m}}{\text{s}}$$

$$f(h) := \frac{(P_2 - 1 \cdot \text{atm})}{\rho} + \frac{v_{13}^2}{2} \frac{1}{C_D^2} + g \cdot h$$

$$h_0 := -1 \cdot \text{m} \quad h_{13} := \text{root}(f(h_0), h_0, -0.5 \cdot \text{m}, -2 \cdot \text{m}) = -1.794 \text{ m}$$

Or shut down one strand and adjust head the to  $0.41 \text{ m}$

$$v_3 := 0.75 \cdot v_{13} = 4.727 \frac{\text{m}}{\text{s}} \quad W_3 := 0.75 \cdot W = 18.9 \frac{\text{kg}}{\text{s}}$$

$$f_3(h) := \frac{(P_2 - 1 \cdot \text{atm})}{\rho} + \frac{v_3^2}{2} \frac{1}{C_D^2} + g \cdot h \quad h_3 := -0.5 \cdot \text{m}$$

$$h_3 := \text{root}(f_3(h_3), h_3, -0.3 \cdot \text{m}, -2 \cdot \text{m}) = -0.41 \text{ m}$$